

PERFORMANCE OF SUBSURFACE DRAINAGE SYSTEMS UNDER VARYING DESIGN AND SOIL PARAMETERS

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Abstract

One of the most important factors for appropriate performance of subsurface drainage systems is having adequate discharge for drains. For this purpose, knowledge about effect of drainage parameters change on drain discharge is essential in subsurface drainage systems. In this article, using change all of the drainage parameters by EnDrain software, changes of drains discharge has been investigated in subsurface drainage systems. The most amount of change in drain discharge for one percent increase or decrease in each of drainage parameters was owned by depth of water level in drain below soil surface equal to 3.0%. Also about maximum and minimum of obtained drain discharge for drainage parameters change has been discussed.

Keywords: Drain discharge, subsurface drainage systems design, water table control

Introduction

The subsurface drainage discharge is one of the most important indicators of the impact of the drainage systems on the water management. Many researches have been done about effect of drainage parameters and correct design of subsurface drainage, which some of them will be described in the following.

Rimidis and Dierickx (2003) evaluated subsurface drainage performance in Lithuania. Oosterbaan (1988) studied agricultural criteria for subsurface drainage. Endres et al. (2007) compared analytical model predictions and field measurements for pumping-induced vadose zone drainage and storage in an unconfined aquifer. The delayed drainage models predicted a relatively rapid dissipation of the undrained storage while the observed undrained storage exhibited little, if any, decay throughout the entire pumping test. Their results indicated that the water table boundary conditions used in these analytical models did not adequately replicate the mechanisms controlling the vadose zone behavior during a pumping test. Cooke et al. (2001) studied drainage equations for random and irregular tile drainage systems. The results predicted by the derived solution were found to be in close agreement with those obtained from the numerical simulations. Therefore, it was concluded that the proposed model holds well for situations of practical import and could be used in future work with large-scale hydrologic models. Howell et al. (2012) presented centrifuge modeling of prefabricated vertical drains for liquefaction remediation. Geng et al. (2012) presented analytical solutions for a single vertical drain with vacuum and time-dependents preloading in membrane and membraneless systems. The analytical solutions improved the accuracy of predicting the dissipation of pore water pressure and the associated settlement. Ghandeharioon et al. (2010) analyzed soil

disturbance associated with mandrel-driven prefabricated vertical drains using an elliptical cavity expansion theory. Basu and Prezzi (2010) designed charts for vertical drains considering soil disturbance. The designed charts could also be used for conditions in which overlapping of disturbed zones occurs. Prasad et al. (2010) estimated unsaturated hydraulic parameters from infiltration and internal drainage experiments. Marinucci et al. (2010) evaluated the effectiveness of prefabricated vertical drains using full-scale in situ staged dynamic testing. Singh (2010) survived generalized analytical solutions for groundwater head in inclined aquifers in the presence of subsurface drains. Oosterbaan (2010) survived role of water harvesting and agricultural land development in spate irrigation in the NWFR of Pakistan. Coles (1968) investigated some notes on drainage design procedure. He showed that various formulae could be solved directly, but graphs have been included to simplify the solution of the different equations. Oosterbaan (1991) studied application of agricultural land drainage. Oosterbaan (1991) in another research discussed about effectiveness and social/environmental impacts of irrigation projects. Samani et al. (2004) studied flow to horizontal and slanted drains in anisotropic unconfined aquifers. Youngs (1986) discussed about water-table heights in drained anisotropic homogeneous soils. Barua and Tiwari (1995) presented theories of seepage into auger holes in homogeneous anisotropic soil. Singh et al. (1996) researched unsteady state drainage in a vertically heterogeneous soil. Endres et al. (2007) compared analytical model predictions and field measurements for pumping-induced vadose zone drainage and storage in an unconfined aquifer. The delayed drainage models predicted a relatively rapid dissipation of the undrained storage while the observed undrained storage exhibited little, if any, decay throughout the entire pumping test. Their results indicated that the water table boundary conditions used in these analytical models did not adequately replicate the mechanisms controlling the vadose zone behavior during a pumping test. Luan and Leng (2008) compared monotonic shear behaviors of granular soils under different drainage conditions. Ali (2011) studied drainage of agricultural lands as a comprehensive research. O'Kelly (2006) compared anisotropy of some soft soils. Gallichand (1994) presented numerical simulations of steady-state subsurface drainage with vertically decreasing hydraulic conductivity. The results presented could be used to estimate the error on watertable depth resulting from ignoring the vertical variations of hydraulic conductivity. Hunt (2005) discussed about flow to vertical and nonvertical wells in leaky aquifers. Choudhry et al. (1995) showed Physical and hydraulic properties of synthetic envelopes for subsurface drainage in Pakistan. Hanson and Ayars (2002) presented strategies for reducing subsurface drainage in irrigated agriculture through improved irrigation. Kannan (2008) Studied drawdown–drain discharge relationship and its application in design of Ccost effective subsurface drainage system in Mugogo Swamp, Busogo, Rwanda. Osiensky et al. (2000) evaluated drawdown curves derived from multiple well aquifer tests in heterogeneous environments. Moustafa (1998) survived time-dependent drainage from root zone and drainage coefficient under different irrigation management levels for subsurface drainage design in Egypt. O'Neill et al. (1989) presented agricultural subsurface drainage from potato fields in northwestern New Brunswick, Canada. Wahba and Christen (2006) modeled subsurface drainage for salt load management in southeastern Australia. Hornbuckle et al. (2005) managed controlled water table management as a strategy for reducing salt loads from subsurface drainage under perennial agriculture in semi-arid Australia. Results from the experiment showed that controlled drainage

significantly reduced drainage volumes and salt loads compared to unmanaged systems. However, there were marked increases in soil salinity which will need to be carefully monitored and managed. Christen et al. (2001) designed subsurface drainage in irrigated areas of Australia, successfully. Castanheira and Santos (2009) presented a simple numerical analyses software for predicting water table height in subsurface drainage. The results obtained with the model agree well with Khirkam's and Hooghoudt analytical solution for the distribution of total head in ideal drains and for the total head calculations midway between drains. Burdon (1986) investigated hydrogeological aspects of agricultural drainage in Ireland, successfully. Ahmadi (1995) using a field approach estimated drainage coefficients in humid area. Brandyk et al. (1992) using a simple flow resistance model managed drainage/sub-irrigation systems. Wesseling (1964) compared the steady state drain spacing formulas of Hooghoudt and Kirkham in connection with design practice. Molen and Wesseling (1991) presented a solution in closed form and a series solution to replace the tables for the thickness of the equivalent layer in Hooghoudt's drain spacing formula. Wesseling (1964) studied the effect of using continually submerged drains on drain spacing. Singh et al. (1992) survived modified steady state drainage equations for transient conditions in subsurface drainage. Lovell and Youngs (1984) compared steady-state land-drainage equations. Of the drainage equations Houghoudt's equivalent depth equation, when used with the optimum drain radius given by the hodograph analysis for infinite soil depth, was the only one that gives results contained mainly within the known bounds that result from a consideration of the combination of equations. Youngs (1985) presented a simple drainage equation for predicting water-table drawdowns. This simple equation was useful in the analysis of falling water tables in drained lands. Singh et al. (1999) survived subsurface drainage of a three layered soil with slowly permeable top layer. The study showed that the watertable head gets influenced by the location of interface between the soil layers. French and O'Callaghan (1966) described a field-test of drain spacing equations for agricultural land. Wiskow and Ploeg (2003) calculated drain spacing for optimal rainstorm flood control. Hirekhan et al. (2007) showed application of WaSim to assess performance of a subsurface drainage system under semi-arid monsoon climate. It appeared that WaSim was a simple tool to evaluate the hydraulic performance of the subsurface drainage systems or to design a subsurface drainage system for semi-arid monsoon climates. Prasher et al. (1994) designed water table management systems in humid areas as economical. Nwa and Twocock (1969) discussed about drainage design theory and practice. Skagges et al. (2006) studied drainage design coefficients for eastern United States. Singh and O'Callaghan (1978) investigated non-steady drainage in a layered soil. Youngs (1986) determined the variation of hydraulic conductivity with depth in drained lands and the design of drainage installations. Gureghian and Youngs (1975) using finite-element method calculated steady-state watertable heights in drained soils. Youngs (1991) in other research said a note on the power-law land-drainage equation for deep soils. Valipour (2012) compared two types subsurface drainage system (horizontal and vertical) in anisotropic soils. He showed that changes of hydraulic conductivity had a significant effect on drain spacing. Most previous studies focused on drainage spacing and neglected role of all drainage parameters in subsurface drainage systems. In this study, using change all of the drainage parameters by EnDrain software, changes of drains discharge has been investigated in subsurface drainage systems.

Materials And Methods

In this study simulated performance of subsurface drainage by using EnDrain software. The drain discharge calculations in this software were based on the Darcy and waterbalance (water balance, budget) or mass conservation equations. In this paper presented ten different scenarios for each of drainage parameters. For each scenarios amount of drain discharge changes obtained and compared. The eight drainage parameters witch survived effect of their changes on drain discharge were depth watertable midway between drains (Dm), bottom depth of layer below soil surface (D), depth of water level in drain below soil surface (Dw), depth of drain bottom below soil surface (Dd), entrance resistance at the drain (E), maximum width of water body in the drain (W), hydraulic permeability (K), and spacing between the parallel drains (S). The amount of entrance resistance at the drain calculated as follows:

$$E = H_e / Q^* \quad (1)$$

Where H_e is entrance head (m) and Q^* is drain discharge (m^2/day) which as follows:

$$Q^* = R \times S \quad (2)$$

Where R is amount of recharge (m/day).

The initial data were Dm=1.0 m, D=6.3 m, Dw=1.5 m, Dd=1.6 m, E=0.5 day/m, W=0.2 m, K=0.14 m/day, S=65 m and have been highlighted in all of the tables in this paper. For these amounts, drain discharge calculated using EnDrain software equal to 0.0009 m/day.

I. Results And Discussion

Table 1 shows obtained results for change of depth watertable midway between drains.

Table 1. Obtained results for change of depth watertable midway between drains (Dm)

Dm (m)	D (m)	Dw (m)	Dd (m)	E (day/m)	W (m)	K (m/day)	S (m)	Drain discharge (m/day)	$\Delta Q/Q$ (%)	$\Delta Dm/Dm$ (%)	Final change (%)
0.1	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0030	233	90	2.6
0.2	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0027	200	80	2.5
0.4	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0022	144	60	2.4
0.6	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0018	100	40	2.5
0.8	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0013	44	20	2.2
1.0	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0009	0	0	0.0
1.1	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0007	22	10	2.2
1.2	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0005	44	20	2.2
1.3	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0004	56	30	1.9
1.4	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0001	89	40	2.2
Average (%)									104	43	2.3

According to the Table 1 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 233% and related to the 90 percent of decreasing depth watertable midway between drains into the initial D_m ($\Delta D_m/D_m$). The minimum of changes was 22% for 10% increasing of D_m .

The amount of final change calculated by dividing $\Delta Q/Q$ on $\Delta D_m/D_m$ therefore amount of 2.3 in Table 1 indicates that as average for one percent decrease or increase in D_m , amount of drain discharge is changed 2.3%. Table 2 shows obtained results for bottom depth of layer below soil surface.

Table 2. Obtained results for bottom depth of layer below soil surface (D)

$D_m(m)$ (m/day)	(mD) (m/day)	$(Dw m)$ $\Delta Q/Q$ (%)	$(Dd m)$ $\Delta D/D$ (%)	(day/mE) change (%)	$(W m)$ Final	$(m/dayK)$	(mS)	Drain	discharge
1.0	2.0							0.000	7 68 1.
								2	8 1
1.0	4.0	1. 1.	1.5 1.6	0.5 0.2	0.14 0.14	60.	6	0.000	3 37 0.
	6.3	5 6		0.5		2	5	6	3 9
1.0		1. 1.	0.5			0. 0.1	6	0.000	0 0 0.
		5 6				2 4	5	9	0
1.0	8.0	1. 1.	0.5			0. 0.1	6	0.001	2 27 0.
		5 6				2 4	5	1	2 8
1.0	10.	1. 1.	0.5			0. 0.1	6	0.001	3 59 0.
	0	5 6				2 4	5	2	3 6
1.0	15.	1. 1.	0.5			0. 0.1	6	0.001	5 13 0.
	0	5 6				2 4	5	4	6 8 0
1.0	20.	1. 1.	0.5			0. 0.1	6	0.001	6 21 0.
	0	5 6				2 4	5	5	7 7 3
1.0	30.	1. 1.	0.5			0. 0.1	6	0.001	6 37 0.
	0	5 6				2 4	5	5	7 6 2
1.0	40.	1. 1.	0.5			0. 0.1	6	0.001	6 53 0.
	0	5 6				2 4	5	5	7 5 1
1.0	50.	1. 1.	0.5			0. 0.1	6	0.001	6 69 0.
	0	5 6				2 4	5	5	7 4 1
Avera									5 23 0.
ge (%)									4 9 5

According to the Table 2 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 78% and related to the 68% decreasing bottom depth of layer below soil surface into the initial D ($\Delta D/D$). The minimum of changes was 22% for 27% increasing of D_m . As average for one percent decrease or increase in D , amount of drain discharge is changed 0.5%.

Table 3 shows obtained results for depth of water level in drain below soil surface.

Table 3. Obtained results for depth of water level in drain below soil surface (Dw)

Dm (m)	D _(m)	Dw _(m)	Dd _(m)	E	W	K	S	Drain discharge	$\Delta Q/Q$	$\Delta Dw/Dw$	Final change (m)	(day/m)	(m)	(m/day)	(m)	(m/day)
1.0	6.3	1.05		0.21	1.6	0.14	0.5	65					0.0001	89	30	3.0
1.0		6.3			1.10	1.6	0.5	0.2	0.14	65			0.0002	78	27	2.9
1.0		6.3			1.15	1.6	0.5	0.2	0.14	65			0.0002	78	23	3.3
1.0		6.3			1.20	1.6	0.5	0.2	0.14	65			0.0003	67	20	3.3
1.0		6.3			1.25	1.6	0.5	0.2	0.14	65			0.0003	67	17	4.0
1.0		6.3			1.30	1.6	0.5	0.2	0.14	65			0.0006	33	13	2.5
1.0		6.3			1.40	1.6	0.5	0.2	0.14	65			0.0008	11	7	1.7
1.0		6.3			1.45	1.6	0.5	0.2	0.14	$\frac{65}{65}$			0.0009	0	3	0.0
1.0		6.3	1.50			1.6	0.5	0.2	0.14				0.0009	0	0	0.0
1.0		6.3			1.55	1.6	0.5	0.2	0.14	65			0.0011	22	3	6.7
Average														49	16	3.0
e (%)																

(%) (%) (%)

According to the Table 3 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 89% and related to the 30% decreasing depth of water level in drain below soil surface into the initial Dw ($\Delta Dw/Dw$). The minimum of changes was 0% for 3% decreasing of Dw. As average for one percent decrease or increase in Dw, amount of drain discharge is changed 3.0%.

Table 4 shows obtained results for depth of drain bottom below soil surface.

Table 4. Obtained results for depth of drain bottom below soil surface (Dd)

Dm (m)	D	D _(m)	Dd (m)	E (day/m)	W (m)	K (m/day)	S (m)	Drain discharge (m/day)	$\Delta Q/Q$ (%)	$\Delta Dd/D$ (%)	Final change (%)
1.0		$\frac{(m)}{6.3}$	1.5	1.6	0.5	0.2	0.14	65	0.0009	0	0.0
1.0		6.3	1.5	1.7	0.5	0.2	0.14	65	0.0010	11	1.8
1.0		6.3	1.5	1.8	0.5	0.2	0.14	65	0.0010	11	0.9
1.0		6.3	1.5	1.9	0.5	0.2	0.14	65	0.0010	11	0.6
1.0		6.3	1.5	2.0	0.5	0.2	0.14	65	0.0011	22	0.9
1.0		6.3	1.5	2.2	0.5	0.2	0.14	65	0.0011	22	0.0
1.0		6.3	1.5	2.5	0.5	0.2	0.14	65	0.0011	22	0.4
1.0		6.3	1.5	3.0	0.5	0.2	0.14	65	0.0012	33	0.4
1.0		6.3	1.5	3.5	0.5	0.2	0.14	65	0.0012	33	0.0

1.0	6.3	1.5	4.0	0.5	0.2	0.14	65	0.0013	44	150	0.3
Average (%)									23	57	0.6

According to the Table 4 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 44% and related to the 150% increasing depth of drain bottom below soil surface into the initial Dd ($\Delta Dd/Dd$). The minimum of changes was 11% for 6-19% increasing of Dd. As average for one percent decrease or increase in Dd, amount of drain discharge is changed 0.6%.

Table 5 shows obtained results for entrance resistance at the drain.

Table 5. Obtained results for entrance resistance at the drain (E)

Dm (m)	D	Dw	Dd	E	W	K	S	Drain discharge	$\Delta Q/Q$	$\Delta E/E(\%)$	Final
Average (%)								1	98	0.0	

change

(m) (m) (m) (day/m) (m) (m/day) (m) (m/day) (%) (%)

According to the Table 5 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 11%

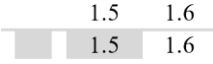
1.0	6.3	1.5	1.6	0.0	0.2	0.14	65	0.0010	11	100	0.1
1.0	6.3	1.5	1.6	0.2	0.2	0.14	65	0.0009	0	60	0.0
1.0	6.3	1.5	1.6	0.4	0.2	0.14	65	0.0009	0	20	0.0
1.0	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0009	0	0	0.0
1.0	6.3	1.5	1.6	0.6	0.2	0.14	65	0.0009	0	20	0.0
1.0	6.3	1.5	1.6	0.8	0.2	0.14	65	0.0009	0	60	0.0
1.0	6.3	1.5	1.6	1.0	0.2	0.14	65	0.0009	0	100	0.0
1.0	6.3	1.5	1.6	1.2	0.2	0.14	65	0.0009	0	140	0.0
1.0	6.3	1.5	1.6	1.4	0.2	0.14	65	0.0009	0	180	0.0
1.0	6.3	1.5	1.6	1.5	0.2	0.14	65	0.0009	0	200	0.0

and related to the 100% decreasing entrance resistance at the drain into the initial E ($\Delta E/E$). The minimum of changes was 0% for other increasing or decreasing of E. As average for one percent decrease or increase in E, amount of drain discharge is changed 0.0%. This indicated that entrance resistance had minimum of effect on drain discharge into the other drainage parameters.

Table 6 shows obtained results for maximum width of water body in the drain.

Table 6. Obtained results for maximum width of water body in the drain (W)

Dm (m)	D (m)	Dw (m)	Dd (m)	E (day/m)	W (m)	K (m/day)	S (m)	Drain discharge (m/day)	$\Delta Q/Q$ (%)	$\Delta W/W(\%)$	Final change (%)
--------	-------	--------	--------	-----------	-------	-----------	-------	-------------------------	------------------	------------------	------------------

1.0	6.	1.5	1.	0.5	0.0	0.14	65	0.0009	0	90	0.0
	3		6		2						
1.0	6.	1.5	1.	0.5	0.0	0.14	65	0.0009	0	75	0.0
	3		6		5						
1.0	6.	1.5	1.	0.5	0.1	0.14	65	0.0009	0	50	0.0
	3		6		0						
1.0	6.			0.5	0.1	0.14	65	0.0009	0	25	0.0
	3				5						
1.0	6.			0.5	0.2	0.14	65	0.0009	0	0	0.0
	3				0						
1.0	6.	1.5	1.	0.5	0.2	0.14	65	0.0010	11	25	0.4
	3		6		5						
1.0	6.	1.5	1.	0.5	0.3	0.14	65	0.0010	11	50	0.2
	3		6		0						
1.0	6.	1.5	1.	0.5	0.3	0.14	65	0.0010	11	75	0.1
	3		6		5						
1.0	6.	1.5	1.	0.5	0.4	0.14	65	0.0010	11	100	0.1
	3		6		0						
1.0	6.	1.5	1.	0.5	0.5	0.14	65	0.0010	11	150	0.1
	3		6		0						
Average (%)									6	71	0.1

According to the Table 6 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 11% and related to the increasing maximum width of water body in the drain into the initial W ($\Delta W/W$). The minimum of changes was 0% for decreasing of W . As average for one percent decrease or increase in W , amount of drain discharge is changed 0.1%.

Table 7 shows obtained results for hydraulic permeability.

Table 7. Obtained results for hydraulic permeability (K)

Dm (m)	D (m)	Dw (m)	Dd (m)	E (day/m)	W (m)	K (m/day)	S (m)	Drain discharge (m/day)	$\Delta Q/Q$ (%)	$\Delta K/K$ (%)	Final change (%)
1.0	6.3	1.5	1.6	0.5	0.2	0.01	65	0.0001	89	93	1.0
1.0	6.3	1.5	1.6	0.5	0.2	0.05	65	0.0003	67	64	1.0
1.0	6.3	1.5	1.6	0.5	0.2	0.14	65	0.0009	0	0	0.0
1.0	6.3	1.5	1.6	0.5	0.2	0.20	65	0.0013	44	43	1.0
1.0	6.3	1.5	1.6	0.5	0.2	0.50	65	0.0036	300	257	1.2

1.0	6.3	1.5	1.6	0.5	0.2	1.00	65	0.0065	622	614	1.0
1.0	6.3	1.5	1.6	0.5	0.2	2.00	65	0.0108	1100	1329	0.8
1.0	6.3	1.5	1.6	0.5	0.2	5.00	65	0.0170	1789	3471	0.5
1.0	6.3	1.5	1.6	0.5	0.2	7.00	65	0.0196	2078	4900	0.4
1.0	6.3	1.5	1.6	0.5	0.2	10.00	65	0.0221	2356	7043	0.3
Average									938	1979	0.8
(%)											

According to the Table 7 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 2356% and related to the 7043% increasing hydraulic permeability into the initial K ($\Delta K/K$). The minimum of changes was 44% for 43% increasing of K. As average for one percent decrease or increase in K, amount of drain discharge is changed 0.8%.

Table 8 shows obtained results for spacing between the parallel drains.

Table 8. Obtained results for spacing between the parallel drains (S)

Dm (m)	D Dw	Dd E	W K S	Drain	discharge	$\Delta Q/Q$	$\Delta S/S(\%)$	Final	change	(m)	(m)	(m)	(day/m)	(m)	(m/day)	(m)
(m/day)	(%)	(%)														
1.0	6.	1.	1.										0.004	40	62	6.
	3	5	6										5	0		5
1.0	6.	1.	1.			0.5	0.2	0.14	25				0.001	89	31	2.
	3	5	6			0.5	0.2	0.14	45				7			9
						0.5	0.2	0.14	65							
1.0	6.	1.	1.										0.000	0	0	0.
	3	5	6										9			0
1.0	6.	1.	1.	0.	0.2					0.1	85	0.000	33	31	1.	
	3	5	6	5						4		6				1
1.0	6.	1.	1.	0.	0.2					0.1	10	0.000	56	54	1.	
	3	5	6	5						4	0	4				0
1.0	6.	1.	1.	0.	0.2					0.1	15	0.000	78	13	0.	
	3	5	6	5						4	0	2		1	6	
1.0	6.	1.	1.	0.	0.2					0.1	20	0.000	89	20	0.	
	3	5	6	5						4	0	1		8	4	
1.0	6.	1.	1.	0.	0.2					0.1	25	0.000	89	28	0.	
	3	5	6	5						4	0	1		5	3	
1.0	6.	1.	1.	0.	0.2					0.1	30	0.000	89	36	0.	
	3	5	6	5						4	0	1		2	2	
1.0	6.	1.	1.	0.	0.2					0.1	40	0.000	89	51	0.	
	3	5	6	5						4	0	1		5	2	

Average	11	18	1.
e (%)	2	6	5

According to the Table 8 maximum amount of drain discharge change into the initial discharge ($\Delta Q/Q$) was 400% and related to the 62% decreasing drain spacing into the initial S ($\Delta S/S$). The minimum of changes was 33% for 31% increasing of S . As average for one percent decrease or increase in S , amount of drain discharge is changed 1.5%. According to the Tables 1-8, the most amount of change in drain discharge for one percent increase or decrease in each of drainage parameters was owned by depth of water level in drain below soil surface (D_w) equal to 3.0%.

Figure 1 shows trends of drain discharge changes for change of each drainage parameters in subsurface drainage systems.

For increasing D_m , amount of drain discharge decreased with an almost uniform slope. The amounts of drain discharge increased for D until 20 meters. After this amount, drain discharge remained constant. For increasing of D_w , D_d , and K , amount of drain discharge also increased. However, entrance resistance caused drain discharge decrease. The amount of $W=0.2$ m (initial situation) was an important point because for amount more than it, drain discharge increased. Where amount of S increased from 25 meters to 45 meters, drain discharge decreased with a steep slope and after 150 meters amount of drain discharge remained constant. Figure 2 shows amounts of minimum, maximum, and average of drain discharge changes for one percent increase or decrease in each of drainage parameters.

In Figure 2 not only the most amount of average changes related to D_w , but minimum and maximum of drain discharge owned by this parameter. Thus, depth of water level in drain below soil surface is introduced as the most effective parameter between all of the drainage parameters for drain discharge. However, should not be ignored role of drain spacing particularly in low spacing's.

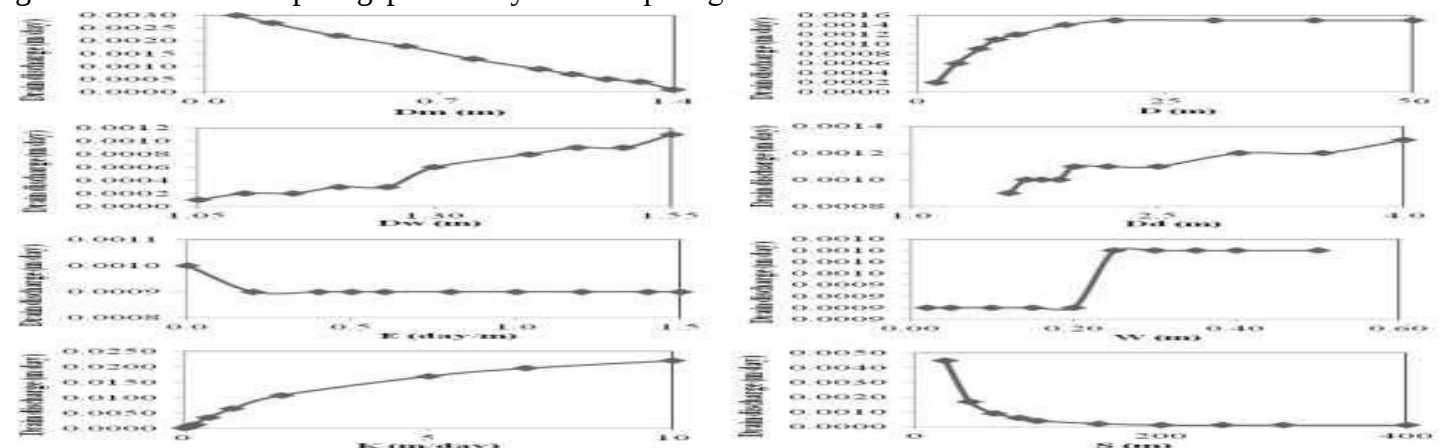


Figure 1. Trends of drain discharge changes for change of each drainage parameters in subsurface drainage systems

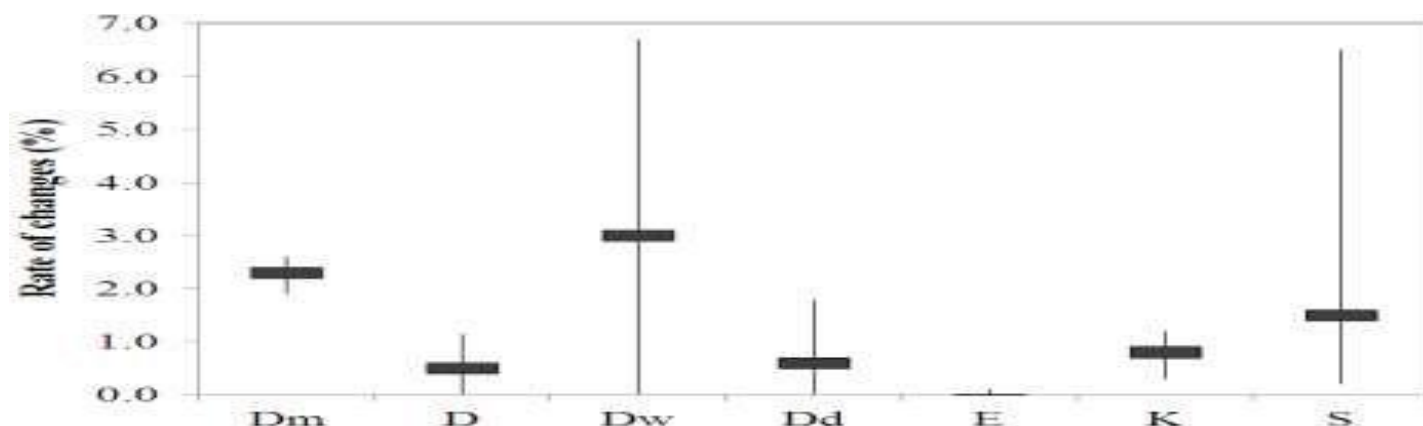


Figure 2. Amounts of minimum, maximum, and average of drain discharge changes for one percent increase or decrease in each of drainage parameters

Conclusion

Due to the importance of subsurface drainage discharge on the water management, in this paper effect of drainage parameters change on amount of drain discharge investigated in subsurface drainage systems. To summarize, it could be concluded that:

Entrance resistance at the drain had minimum of effect on drain discharge into the other drainage parameters.

The most amount of change in drain discharge for one percent increase or decrease in each of drainage parameters was owned by depth of water level in drain below soil surface equal to 3.0%.

When amount of drain spacing increased from 25 meters to 45 meters, drain discharge decreased with a steep slope and after 150 meters amount of drain discharge remained constant.

Depth of water level in drain below soil surface is introduced as the most effective parameter between all of the drainage parameters for drain discharge. However, should not be ignored role of drain spacing particularly in low spacings.

References

- Barua G. and K.N. Tiwari, 1995. Theories of seepage into auger holes in homogeneous anisotropic soil, *Journal of Hydrology*, 167 (1–4), pp. 1–22.
- Basu D. and M. Prezzi 2010. Design Charts for Vertical Drains Considering Soil Disturbance, *Geotechnical Modeling*, pp. 420–429.
- Brandyk T., P.B. Leeds-Harrison and K. Skapski 1992. A simple flow resistance model for the management of drainage/subirrigation systems, *Agricultural Water Management*, 21 (1–2), pp. 67–77.
- Burdon D.J. 1986. Hydrogeological aspects of agricultural drainage in Ireland, *Environmental Geology and Water Sciences*, 9 (1), pp. 41–65